

## Suggested solution - Exam, May 27, 2003

### Problem 1

a) System matrix:

$$\begin{pmatrix} A & B \\ C & D \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ -1/f_2 & 1 \end{pmatrix} \begin{pmatrix} 1 & t \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -1/f_1 & 1 \end{pmatrix} = \begin{pmatrix} 1 - \frac{t}{f_1} & t \\ -\left(\frac{1}{f_1} + \frac{1}{f_2} - \frac{t}{f_1 f_2}\right) & 1 - \frac{t}{f_2} \end{pmatrix}$$

$$= \begin{pmatrix} 1/3 & 16 \text{ cm} \\ -1/48 \text{ cm}^{-1} & 2 \end{pmatrix}$$

Power:  $P = -C = 1/48 \text{ cm}^{-1} = \underline{2.08 \text{ m}^{-1}(\text{diop})}$

b) From a) and  $n = n' = 1$ :  $f = f' = -n/C = \underline{48 \text{ cm}}$ .  $h = (1-D)n/C = \underline{48 \text{ cm}}$ , i.e.,  $H$  is 48 cm to the left of  $L_1$ .  $h' = (1-A)n'/C = \underline{-32 \text{ cm}}$ , i.e.,  $H'$  is 32 cm to the left of  $L_2$ . The front focal point  $F$  is a distance  $f+h = 96 \text{ cm}$  to the left of  $L_1$ . The back focal point  $F'$  is a distance  $f+h' = 16 \text{ cm}$  to the right of  $L_2$ .

c) The object is a distance  $s = 144 \text{ cm} - 48 \text{ cm} = 2f$  to the left of  $H$ . From the lens formula we then see that the image is the same distance  $s' = 2f$  to the right of  $H'$ . The image is located the distance  $h' + 2f = \underline{64 \text{ cm}}$  to the right of  $L_2$ . The magnification is  $\beta = -s'/s = \underline{-1}$ .

d) *The aperture stop* is the physical stop that limits the ray-bundle contributing to the image point on-axis.

*The field stop* is the physical stop that limits the bundle of chief-rays through the center of the aperture stop.

*The entrance pupil* is the aperture stop seen from or imaged into object space.

*The exit pupil* is the aperture stop seen from or imaged into image space.

*The entrance window* is the field stop seen from or imaged into object space.

*The exit window* is the field stop seen from or imaged into image space.

We image all stops to the object space (might as well have chosen the image space):

$L_1$  is in object space (it is imaged onto itself). At the object point on-axis its aperture subtends the angle  $2/144 \text{ rad} = 1/72 \text{ rad}$ . The image of  $L_2$  (formed by imaging through  $L_1$ ) is a distance  $s$  to the left of  $L_1$ , where the lens formula:  $1/s + 1/(16 \text{ cm}) = 1/f_1$  yields  $s = -48 \text{ cm}$ . The image is therefore located 48 cm to the right of  $L_1$  and the magnification is  $48/16 = 4$ . The image of the aperture of  $L_2$  therefore has a diameter of 16 cm and it

subtends the angle  $8/(144+48) \text{ rad} = 1/21 \text{ rad}$  at the object point on axis. *The smallest angle is subtended by  $L_1$ , which is therefore the aperture stop.*

(This can also be seen directly: the object distance is larger than  $f_1$  and then  $L_1$  will serve to *converge* the ray-bundle from the object point on-axis so that it can never be limited by  $L_2$ ).

The exit pupil is the aperture stop  $L_1$  imaged into image space. Then  $L_1$  is imaged by  $L_2$  to a virtual image at a distance 8 cm to the left of  $L_2$  and with the magnification  $8/16=1/2$ .

*The exit pupil* is therefore 8 cm to the left of  $L_2$  and has a diameter of 2 cm.

$F$ -number in image space:  $F' = (64+8)/2 = \underline{36}$ .

## Problem 2

- a) With a 50/50 beam-splitter each of the two waves has the same intensity  $I_1=I_2=I_0$ , and from the interference equation we then have

$$I(s) = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos(ks) = 2I_0[1 - \cos(ks)] = 2I_0[1 + \cos(\omega s/c)].$$

where we have used that  $k = \omega/c$ .

For a polychromatic source the corresponding contribution to the intensity from the frequency range  $d\omega$  is:  $dI(s) = 2W(\omega)[1 + \cos(\omega s/c)]d\omega$ . Integrating over all frequencies we obtain:

$$I(s) = 2 \int_0^{\infty} W(\omega)[1 + \cos(\omega s/c)]d\omega.$$

From the given formulas we have

$$\Gamma(0) = \int_0^{\infty} W(\omega)d\omega \text{ and } \text{Re}\Gamma(s/c) = \int_0^{\infty} W(\omega)\cos(\omega s/c)d\omega, \text{ which directly yields}$$

$$I(s) = 2[\Gamma(0) + \text{Re}\Gamma(s/c)]. \text{ QED}$$

- b) The visibility is defined as  $V = \frac{I_{\max} - I_{\min}}{I_{\max} + I_{\min}}$ , where  $I_{\max}$  is the maximum intensity

(at constructive interference) and  $I_{\min}$  is the minimum intensity (at destructive interference) of the interference signal.

With the given interference signal, we have  $I_{\max} = 2I_0[1 + \exp(-|s|/L)]$  and

$$I_{\min} = 2I_0[1 - \exp(-|s|/L)], \text{ which yield: } V(s) = \exp(-|s|/L).$$

By direct substitution, we see that the given interference signal is obtained from

$$\Gamma(s/c) = I_0 \exp\left[-(|s|/L + i2\pi s/\lambda_0)\right], \text{ i.e., } \Gamma(\tau) = I_0 \exp\left[-(|\tau|c/L + i2\pi\tau/\lambda_0)\right],$$

which equals the given expression for

$$T = L/c = 1.66666 \cdot 10^{-11} \text{ sec} = 16.6666 \text{ ps}$$

and

$$\omega_0 = 2\pi/\lambda_0 = 3.77 \cdot 10^{15} \text{ rad/s.}$$

- c) We have  $\Gamma(\tau) = \Gamma(0)\gamma(\tau) = I\gamma(\tau)$ , where  $I = \Gamma(0)$  is the total intensity (a constant). The given formulas then yield

$$\begin{aligned} W(\omega) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} \Gamma(\tau) \exp(i\omega\tau) d\tau \\ &= \frac{I_0}{2\pi} \int_{-\infty}^{\infty} \gamma(\tau) \exp(i\omega\tau) d\tau = \frac{I_0}{2\pi} \int_{-\infty}^{\infty} \exp\left[-(|\tau|/T + i(\omega_0 - \omega)\tau)\right] d\tau \end{aligned}$$

Since we have  $|\tau| = \begin{cases} \tau & \text{for } \tau > 0 \\ -\tau & \text{for } \tau < 0 \end{cases}$ , the integral must be subdivided into two parts:

$$\begin{aligned} W(\omega) &= \frac{I_0}{2\pi} \int_{-\infty}^{\infty} \exp\left[-(|\tau|/T + i(\omega_0 - \omega)\tau)\right] d\tau \\ &= \frac{I_0}{2\pi} \int_{-\infty}^0 \exp\left[(1/T - i(\omega_0 - \omega))\tau\right] d\tau + \frac{I_0}{2\pi} \int_0^{\infty} \exp\left[-(1/T + i(\omega_0 - \omega))\tau\right] d\tau \\ &= \frac{I_0}{2\pi} \int_0^{\infty} \left\{ \exp\left[-(1/T - i(\omega - \omega_0))\tau\right] + \exp\left[-(1/T + i(\omega - \omega_0))\tau\right] \right\} d\tau, \end{aligned}$$

where the first term in the last line follows by a simple change of the integration variable ( $\tau \rightarrow -\tau$ ). Direct integration yields

$$W(\omega) = \frac{I_0}{2\pi} \left( \frac{T}{1 + i(\omega - \omega_0)T} + \frac{T}{1 - i(\omega - \omega_0)T} \right) = \frac{I_0 T}{\pi} \frac{1}{1 + [(\omega - \omega_0)T]^2}.$$

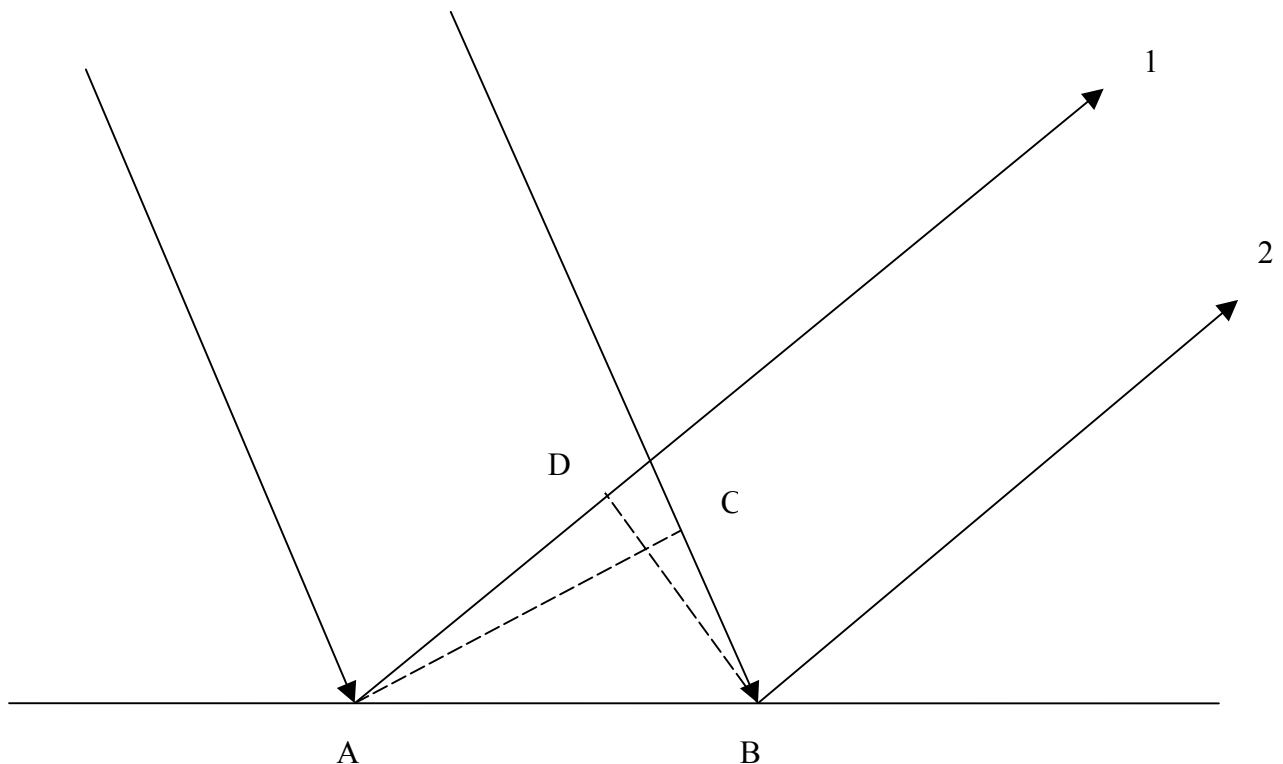
- d) The maximum is  $W(\omega_0) = I_0 T / \pi$  at the center frequency

$$\omega = \omega_0 = 3.77 \cdot 10^{15} \text{ rad/s,}$$

and the half-width around this maximum is

$$2/T = 1.2 \cdot 10^{11} \text{ rad/s.}$$

(the value is reduced by a factor 1/2 relative to the maximum value at the frequencies  $\omega = \omega_0 \pm 1/T$ ).

**Problem 3**

- a) The rays are marked with arrows. The path-length difference between the two rays (1 and 2) reflected from two neighboring grooves at A and B is  $AD - BC$ , where the dotted lines AC and BD are normal to, respectively, the ray incident at B and the ray reflected at A. For the angles we therefore have:  $\angle BAC = \theta_0$  and  $\angle ABD = \theta$ . With the grating constant  $a = AB$ , we therefore have for the path-length difference:

$$s = AD - BC = a(\sin \theta - \sin \theta_0) \text{ QED!}$$

- b) The light in the two rays are in-phase if  $s = m\lambda$  where  $m = 0, \pm 1, \pm 2, \dots$  etc. and  $\lambda$  is the wavelength. Then the light reflected from any two grooves are also in-phase, so that the reflected waves from all the grooves interfere constructively. Therefore the diffraction orders are in the directions  $\theta = \theta_m$  where  $\theta_m$  is given by the *grating equation*:

$$a(\sin \theta_m - \sin \theta_0) = m\lambda; m = 0, \pm 1, \pm 2, \dots \text{etc.}$$

- c) For the order at the height  $h=0$ , we have

$$m_{\max} = \frac{a}{\lambda} [\sin(\pi/2) - \sin \theta_0] = \frac{a}{\lambda} [1 - \sin(\arctan(500/30))],$$

and for the order closest to  $h = 3h_0$  we have

$$m_{\min} = \frac{a}{\lambda} [\sin(\arctan(500/90)) - \sin(\arctan(500/30))].$$

The difference is

$$m_{\max} - m_{\min} = \frac{a}{\lambda} [1 - \sin(\arctan(500/90))] = 24.987$$

We therefore have 24 diffraction orders with a height  $< 3h_0$ .

- d) We now have  $U(x, y, 0) = At(x) = \frac{A}{2} [1 + \cos(2\pi x/a)]$  and obtain for the Fourier spectrum at  $z = 0$ :

$$A(u, v, 0) = 2\pi AT(u)\delta(v),$$

where

$$T(u) = F\{t(x)\} = 2\pi A [\delta(u) + \frac{1}{2} \{\delta(u - 2\pi/a) + \delta(u + 2\pi/a)\}]$$

because  $F\{1\} = 2\pi\delta(u)$  and  $F\{\cos(\alpha x)\} = \pi[\delta(u - \alpha) + \delta(u + \alpha)]$  (see Øving 12 and Eq.(1.3) in the lecture notes). The angular spectrum representation of the diffracted field (Eq. (2.9) in the notes) then yields:

$$\begin{aligned} U(x, y, z) &= \left(\frac{1}{2\pi}\right)^2 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} A(u, v, 0) \exp[i(ux + vy + z\sqrt{k^2 - u^2 - v^2})] dudv \\ &= A \int_{-\infty}^{\infty} [\delta(u) + \frac{1}{2} \{\delta(u - 2\pi/a) + \delta(u + 2\pi/a)\}] \delta(v) \exp[i(ux + vy + z\sqrt{k^2 - u^2 - v^2})] dudv. \end{aligned}$$

Here we have contributions for  $v = 0$  and  $u = 0, \pm 2\pi/a$ , which give rise to only three plane waves:

$$U(x, y, z) = A \exp(ikz) + \frac{1}{2} A \exp\left[i\left(\frac{2\pi x}{a} + z\sqrt{k^2 - \left(\frac{2\pi}{a}\right)^2}\right)\right] + \frac{1}{2} A \exp\left[i\left(-\frac{2\pi x}{a} + z\sqrt{k^2 - \left(\frac{2\pi}{a}\right)^2}\right)\right]$$

The first term is a plane wave in the  $z$  direction, the two last terms are plane waves propagating at angles  $\pm \theta$  with the  $z$  axis. Since  $A \exp[ik(x \sin \theta + z \cos \theta)]$  describes a

plane wave at an angle  $\theta$  with the axis, we see that  $\sin \theta = \frac{2\pi}{ka} = \frac{\lambda}{a}$ . QED!

For  $a < \lambda$ , the factor  $\sqrt{k^2 - \left(\frac{2\pi}{a}\right)^2} = 2\pi\sqrt{1/\lambda^2 - 1/a^2} = \frac{2\pi i}{a}\sqrt{1 - (a/\lambda)^2}$  becomes

purely imaginary, so that the two last plane waves are exponentially damped in the  $z$ -direction.

