

4. Rigid body kinematics

(53)

4.1 Independent coordinates

N particles $\Rightarrow 3N$ degrees of freedom

Holonomic constraints: $r_{ij} = C_{ij}$ [$\frac{1}{2}N(N-1)$ constraints]

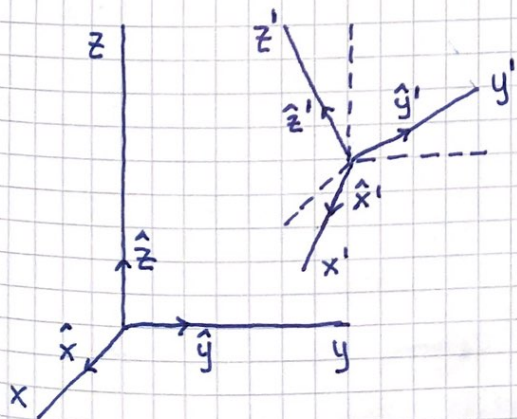
$\Rightarrow$ Only 6 degrees of freedom:

- 3 coords. to specify a reference point in the rigid body (e.g. CM)
- 3 coords. ^(angles) to specify orientation of the rigid body relative to the chosen reference frame

Alternatively:

6 independent movements, translation along 3 axes and rotation around 3 axes.

Let x, y, z be axes in a fixed (external) coord. system, and x', y', z' axes in a coord. system fixed in the rigid body:



3 coords. specify the origin in the $(x' y' z')$ system.

$\Rightarrow$ Need 3 more to specify the directions of x', y', z' relative to x, y, z

(54)

Direction cosines :

$$\alpha_1 = \cos(\hat{x}', \hat{x}) = \hat{x}' \cdot \hat{x}$$

$$\alpha_2 = \cos(\hat{x}', \hat{y}) = \hat{x}' \cdot \hat{y}$$

$$\alpha_3 = \cos(\hat{x}', \hat{z}) = \hat{x}' \cdot \hat{z}$$

Similarly with β for $\hat{y}'$ and γ for $\hat{z}'$.The direction cosines are the components of $\hat{x}', \hat{y}', \hat{z}'$ along the external axes $\hat{x}, \hat{y}, \hat{z}$:

$$\hat{x}' = \alpha_1 \hat{x} + \alpha_2 \hat{y} + \alpha_3 \hat{z}$$

$$\hat{y}' = \beta_1 \hat{x} + \beta_2 \hat{y} + \beta_3 \hat{z}$$

$$\hat{z}' = \gamma_1 \hat{x} + \gamma_2 \hat{y} + \gamma_3 \hat{z}$$

And the other way around :

$$\hat{x} = \alpha_1 \hat{x}' + \beta_1 \hat{y}' + \gamma_1 \hat{z}'$$

$$\hat{y} = \alpha_2 \hat{x}' + \beta_2 \hat{y}' + \gamma_2 \hat{z}'$$

$$\hat{z} = \alpha_3 \hat{x}' + \beta_3 \hat{y}' + \gamma_3 \hat{z}'$$

6 constraints reduce 9 direction cosines to 3 independent coordinates :

$$\hat{x} \cdot \hat{x} = (\alpha_1 \hat{x}' + \beta_1 \hat{y}' + \gamma_1 \hat{z}')^2 = \alpha_1^2 + \beta_1^2 + \gamma_1^2 = 1$$

$$\hat{x} \cdot \hat{y} = \alpha_1 \alpha_2 + \beta_1 \beta_2 + \gamma_1 \gamma_2 = 0$$

etc.

$$\Rightarrow \alpha_i \alpha_j + \beta_i \beta_j + \gamma_i \gamma_j = \delta_{ij}$$

Soon: Euler angles, 3 independent functions of the direction cosines

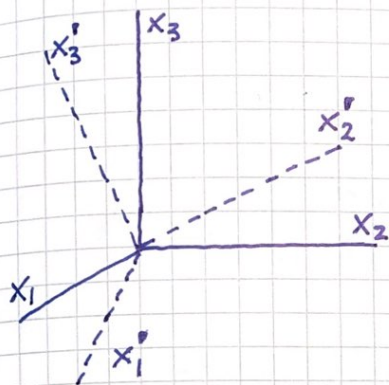
4.2 Orthogonal transformations

(55)

Focus on rotation.

Assume common origin in external and body system.

Notation: $x, y, z \rightarrow x_1, x_2, x_3$ (more convenient)



Coord. transformations:

$$x'_1 = \alpha_1 x_1 + \alpha_2 x_2 + \alpha_3 x_3$$

$$x'_2 = \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3$$

$$x'_3 = \gamma_1 x_1 + \gamma_2 x_2 + \gamma_3 x_3$$

i.e., a linear transf.

General notation:

$$x'_1 = a_{11} x_1 + a_{12} x_2 + a_{13} x_3$$

$$x'_2 = a_{21} x_1 + a_{22} x_2 + a_{23} x_3$$

$$x'_3 = a_{31} x_1 + a_{32} x_2 + a_{33} x_3$$

With summation convention:

$$x'_i = a_{ij} x_j \quad ; \quad i=1,2,3 \quad (1)$$

A rotation leaves $r = |\vec{r}|$ unchanged:

$$x'_i x'_i = x_i x_i \Rightarrow a_{ij} x_j a_{ik} x_k = x_i x_i$$

$$\Rightarrow a_{ij} a_{ik} = \delta_{jk} \quad (2)$$

i.e., the 6 constraints on p. 54.

When (2) are satisfied, (1) is called an orthogonal transformation, and (2) is the orthogonality condition.

Transformation matrix:

$$A = \begin{pmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{pmatrix}$$

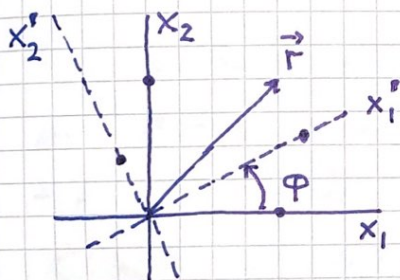
with matrix elements a_{ij}

Ex: Rotation in 2D

$$A = \begin{pmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{pmatrix} ; \quad a_{ij} a_{ik} = \delta_{jk}$$

4 matrix elements, 3 orthog. conditions

$\Rightarrow$ 1 independent coordinate, the rotation angle φ , OK!



From the figure (check yourself):

$$x_1' = x_1 \cos \varphi + x_2 \sin \varphi$$

$$x_2' = -x_1 \sin \varphi + x_2 \cos \varphi$$

$$\Rightarrow a_{11} = a_{22} = \cos \varphi ; \quad a_{12} = -a_{21} = \sin \varphi$$

$$\Rightarrow A = \begin{pmatrix} \cos \varphi & \sin \varphi \\ -\sin \varphi & \cos \varphi \end{pmatrix}$$

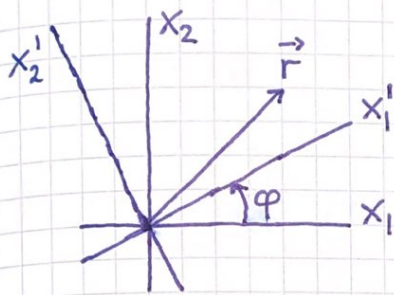
Orthog. conditions:

$$\left. \begin{array}{ll} j=k=1: & a_{11} a_{11} + a_{21} a_{21} = 1 \Rightarrow \cos^2 \varphi + \sin^2 \varphi = 1 \\ j=k=2: & a_{12} a_{12} + a_{22} a_{22} = 1 \Rightarrow \sin^2 \varphi + \cos^2 \varphi = 1 \\ j \neq k: & a_{11} a_{12} + a_{21} a_{22} = 0 \Rightarrow \cos \varphi \sin \varphi - \sin \varphi \cos \varphi = 0 \end{array} \right\} \text{OK!}$$

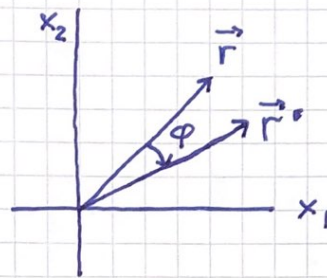
Expressed in 3D, rotation around z axis:

$$A = \begin{pmatrix} \cos \varphi & \sin \varphi & 0 \\ -\sin \varphi & \cos \varphi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Two interpretations of the transformation $\vec{r}' = A\vec{r}$: (57)



Passive



Active

Passive point of view:

Operator A rotates the coord. system, here counterclockwise. Vector $\vec{r}$ is fixed, $\vec{r}'$ expresses components of $\vec{r}$ in rotated coord. system.

Active point of view:

A rotates the vector $\vec{r}$, here clockwise, while the coord. system is fixed. $\vec{r}'$ contains components x_1' and x_2' after the rotation.

4.3 Formal properties of the transformation matrix

(58)

(see also MA1201, MA1202, TMA4115)

Notation: $\vec{r} \rightarrow \vec{x} = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$

- Two successive orthogonal transf. B followed by A equals a single orthog. transf. $C = AB$:

$$x'_k = b_{kj} x_j ; x''_i = a_{ik} x'_k = a_{ik} b_{kj} x_j \equiv C_{ij} x_j$$

$$\Rightarrow C_{ij} = a_{ik} b_{kj} \quad (\text{remember summation convention})$$

- In general, $AB \neq BA$ but $(AB)C = A(BC)$, i.e. orthog. transf. are associative but not commutative.

- The inverse transf. A^{-1} , with matrix elements $\bar{a}_{ij}^{-1}$ (NB: $\bar{a}_{ij}^{-1} \neq 1/a_{ij}$), brings $\vec{x}'$ back to $\vec{x}$:

$$x_i = \bar{a}_{ij}^{-1} x'_j \Rightarrow x'_k = a_{ki} x_i = a_{ki} \bar{a}_{ij}^{-1} x'_j$$

$$\Rightarrow \underbrace{a_{ki} \bar{a}_{ij}^{-1}}_{(A A^{-1})_{kj}} = \underbrace{\delta_{kj}}_{\mathbb{1}_{kj}} \Rightarrow A A^{-1} = \mathbb{1} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\text{Also: } x_i = \bar{a}_{ij}^{-1} x'_j = \bar{a}_{ij}^{-1} a_{jk} x_k \Rightarrow \bar{a}_{ij}^{-1} a_{jk} = \delta_{ik}$$

$$\Rightarrow A^{-1} A = \mathbb{1} \Rightarrow A \text{ and } A^{-1} \text{ commute}$$

- For an orthogonal matrix, $A^{-1} = \tilde{A}$ = transposed of A

Proof: $a_{kl} a_{ki} \bar{a}_{ij}^{-1} = \delta_{il} \bar{a}_{ij}^{-1} = \bar{a}_{lj}^{-1}$ (using orthog. cond.) and $a_{kl} a_{ki} \bar{a}_{ij}^{-1} = a_{kl} \delta_{kj} = a_{lj}$ (using $A A^{-1} = \mathbb{1}$). Hence, $\bar{a}_{lj}^{-1} = a_{lj} = \tilde{a}_{lj}$, i.e., $A^{-1} = \tilde{A}$

(59)

- Alternative expressions for orthog. conditions:

$$\tilde{A}A = \mathbb{1} \Rightarrow \tilde{a}_{ij} a_{jk} = \delta_{ik} \Rightarrow a_{ji} a_{jk} = \delta_{ik}$$

$$A\tilde{A} = \mathbb{1} \Rightarrow a_{ij} \tilde{a}_{jk} = \delta_{ik} \Rightarrow a_{ij} a_{kj} = \delta_{ik}$$

I.e., may sum over 1. or 2. index

- Determinants: $|AB| = |A| \cdot |B|$ (in general)
 $\Rightarrow |\tilde{A}| \cdot |A| = 1$ and since $|\tilde{A}| = |A|$ (—"")
 we find $|A|^2 = 1$, i.e., $|A| = \pm 1$

- The orthog. transf. must be realizable for a rigid body, hence $|A| = +1$

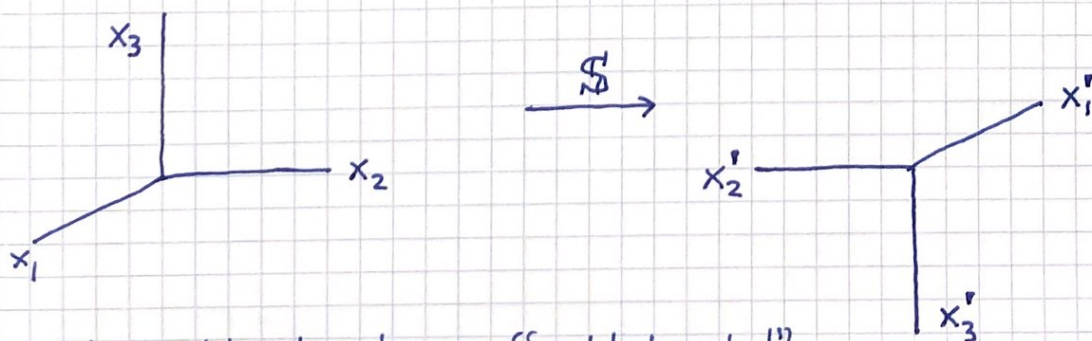
Argument 1: $|A|$ must evolve continuously from the unit matrix $\Rightarrow |A| = |\mathbb{1}| = +1$.

Argument 2, by an example:

Consider the transf. $\vec{x}' = \$ \vec{x}$ with

$$\$ = \begin{pmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{pmatrix} \Rightarrow |\$| = -1$$

i.e. reflection of all 3 axes, $x'_1 = -x_1$ etc.



Not possible to change "right handed" rigid body into a "left handed" one by rotations and translation

4.4 The Euler angles

(60)

We need 3 independent coords. that specify the rigid body orientation, such that $|A| = +1$.

Common choice is the Euler angles, which are 3 successive rotation angles. $A = B C D$

1. Rot. $\varphi > 0$ around z axis, $xyz \rightarrow \xi \eta \zeta$

$$\xi = D x, \quad x = \begin{pmatrix} x \\ y \\ z \end{pmatrix}, \quad \xi = \begin{pmatrix} \xi \\ \eta \\ \zeta \end{pmatrix}$$

$$D = \begin{pmatrix} \cos \varphi & \sin \varphi & 0 \\ -\sin \varphi & \cos \varphi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

2. Rot. $\theta > 0$ around ξ axis, $\xi \eta \zeta \rightarrow \xi' \eta' \zeta'$

$$\xi' = C \xi, \quad \xi' = \begin{pmatrix} \xi' \\ \eta' \\ \zeta' \end{pmatrix}$$

$$C = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & \sin \theta \\ 0 & -\sin \theta & \cos \theta \end{pmatrix}$$

3. Rot. $\psi > 0$ around ζ' axis, $\xi' \eta' \zeta' \rightarrow x' y' z'$

$$x' = B \xi', \quad x' = \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}$$

$$B = \begin{pmatrix} \cos \psi & \sin \psi & 0 \\ -\sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$X' = A X = B C D X$$

(61)

$$\Rightarrow a_{11} = \cos \psi \cos \varphi - \cos \theta \sin \varphi \sin \psi$$

$$a_{12} = \cos \psi \sin \varphi + \cos \theta \cos \varphi \sin \psi$$

$$a_{13} = \sin \psi \sin \theta$$

$$a_{21} = -\sin \psi \cos \varphi - \cos \theta \sin \varphi \cos \psi$$

$$a_{22} = -\sin \psi \sin \varphi + \cos \theta \cos \varphi \cos \psi$$

$$a_{23} = \cos \psi \sin \theta$$

$$a_{31} = \sin \theta \sin \varphi$$

$$a_{32} = -\sin \theta \cos \varphi$$

$$a_{33} = \cos \theta$$

Inverse transformation:

$$X = A^{-1} X' = \tilde{A} X'$$

$$\tilde{a}_{ij} = a_{ji}$$

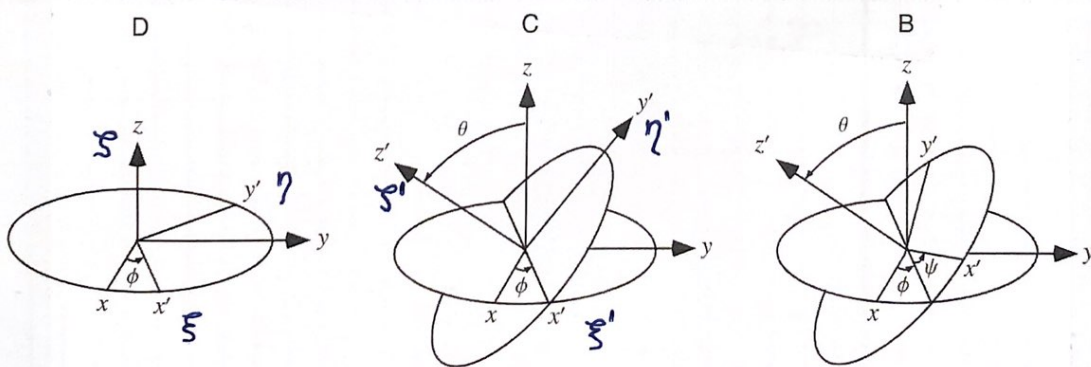


Fig: Wolfram MathWorld (E.W. Weisstein)

4.8 Infinitesimal rotations

In general, two finite rotations A and B do not commute.

Ex.1: $\mathbb{C}$ and $\mathbb{D}$ on p. 60.

Ex.2: Matchbox rotated 90° around two orthogonal axes.

But infinitesimal transformations commute:

$$X_i' = X_i + \epsilon_{ij} X_j = (\delta_{ij} + \epsilon_{ij}) X_j ; \quad \epsilon_{ij} \ll 1$$

On matrix form: $X' = (1 + \epsilon) X$

Two successive inf. transf.:

$$\left. \begin{aligned} (1 + \epsilon_1)(1 + \epsilon_2) &= 1 + \epsilon_1 + \epsilon_2 \\ (1 + \epsilon_2)(1 + \epsilon_1) &= 1 + \epsilon_1 + \epsilon_2 \end{aligned} \right\} \text{commutative!}$$

Inverse inf. transf.:

$$A^{-1} = 1 - \epsilon \quad \text{since} \quad A A^{-1} = (1 + \epsilon)(1 - \epsilon) = 1$$

Orthogonality:

$$\tilde{A} = 1 + \tilde{\epsilon} = A^{-1} \Rightarrow \tilde{\epsilon} = -\epsilon \Rightarrow \tilde{\epsilon}_{ij} = \epsilon_{ji} = -\epsilon_{ij}$$

i.e. ϵ is antisymmetric 3×3 matrix on the form

$$\epsilon = \begin{pmatrix} 0 & d\Omega_3 & -d\Omega_2 \\ -d\Omega_3 & 0 & d\Omega_1 \\ d\Omega_2 & -d\Omega_1 & 0 \end{pmatrix}$$

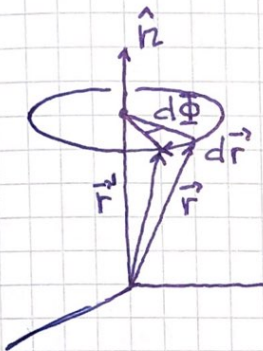
$$\Rightarrow \mathbf{x}' - \mathbf{x} \equiv d\mathbf{x} = \mathbf{\epsilon} \mathbf{x} = \begin{pmatrix} 0 & d\Omega_3 & -d\Omega_2 \\ -d\Omega_3 & 0 & d\Omega_1 \\ d\Omega_2 & -d\Omega_1 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} \quad (63)$$

$$\Rightarrow dx_1 = x_2 d\Omega_3 - x_3 d\Omega_2$$

$$dx_2 = x_3 d\Omega_1 - x_1 d\Omega_3$$

$$dx_3 = x_1 d\Omega_2 - x_2 d\Omega_1$$

$$\Rightarrow d\vec{r} = \vec{r} \times d\vec{\Omega}$$



$$d\vec{r} = \vec{r} \times d\vec{\Omega} ; \quad d\vec{\Omega} = \hat{n} d\Phi$$

NB: $d\vec{\Omega}$ is not the differential of a finite vector $\vec{\Omega}$; $d\vec{\Omega}$ is a differential vector

$d\vec{r} = \vec{r}' - \vec{r}$ = change in the vector produced by an infinitesimal (clockwise) rotation of the vector

4.9 Rate of change of a vector

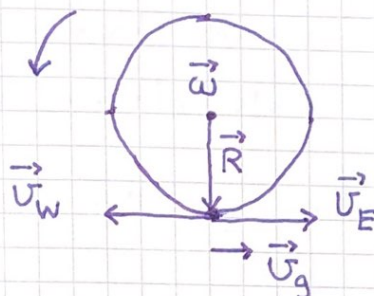
The change $d\vec{G}$ in an arbitrary (general) vector $\vec{G}$ is measured with different values in the ~~the~~ coord. system fixed in the rigid body and the external coord. system:

$$(d\vec{G})_{\text{body}} \neq (d\vec{G})_{\text{space}}$$

The difference due to rotation of the body system in the space system is $\vec{G} \times d\vec{\Omega}$, and we fix the sign with an example.

A car drives east or west on the equator:

(64)



$\vec{\omega} = d\vec{\Omega}/dt$ out of the plane

$\vec{U}_g = \vec{\omega} \times \vec{R}$ = speed of ground measured in fixed external system

$\vec{U}_{E,W}$ = speed of car in rotating system

$$\Rightarrow \vec{U}_c = \vec{U}_{E,W} + \vec{\omega} \times \vec{R}$$

= speed of car in external system

$$\Rightarrow (d\vec{G})_{\text{space}} = (d\vec{G})_{\text{body}} + d\vec{\Omega} \times \vec{G}$$

$$\Rightarrow \left(\frac{d\vec{G}}{dt}\right)_s = \left(\frac{d\vec{G}}{dt}\right)_b + \vec{\omega} \times \vec{G}$$

$\vec{\omega} = d\vec{\Omega}/dt$ = instantaneous angular velocity

Operator relation:

$$\left(\frac{d}{dt}\right)_s = \left(\frac{d}{dt}\right)_b + \vec{\omega} \times$$

Ex: $\vec{G} = \vec{r} \Rightarrow \vec{U}_s = \vec{U}_b + \vec{\omega} \times \vec{r}$ (as above)

(For a more formal derivation of the operator relation, see Goldstein or handwritten compendium.)

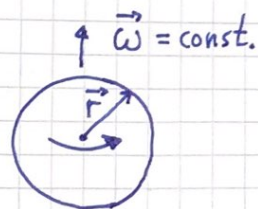
4.10 Coriolis force and centrifugal force

(65)

s = approximate inertial system fixed relative to some nearby stars

b = system rotating with the earth

Assume common axes at a given instant.



$$\vec{G} = \vec{r} \Rightarrow \vec{U}_s = \vec{U}_b + \vec{\omega} \times \vec{r}$$

$$\vec{G} = \vec{U}_s \Rightarrow \left(\frac{d\vec{U}_s}{dt} \right)_s = \left(\frac{d\vec{U}_s}{dt} \right)_b + \vec{\omega} \times \vec{U}_s$$

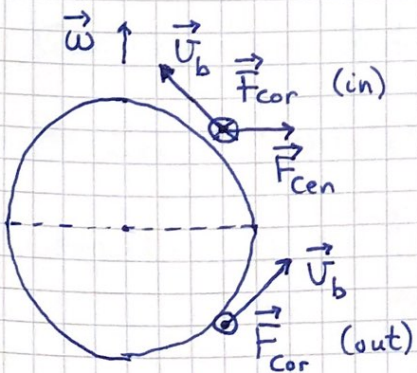
$$\left(\frac{d\vec{U}_s}{dt} \right)_b = \left(\frac{d\vec{U}_b}{dt} \right)_b + \left[\frac{d}{dt} (\vec{\omega} \times \vec{r}) \right]_b = \vec{a}_b + \vec{\omega} \times \vec{U}_b$$

$$\vec{\omega} \times \vec{U}_s = \vec{\omega} \times \vec{U}_b + \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$\Rightarrow \vec{a}_s = \vec{a}_b + 2 \vec{\omega} \times \vec{U}_b + \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

N2 in the inertial frame s , $\vec{F} = m \vec{a}_s$,
can now be expressed as $\vec{F}_b = m \vec{a}_b$ with

$$\vec{F}_b = \vec{F} + \underbrace{2m \vec{U}_b \times \vec{\omega}}_{\text{Coriolis force}} - \underbrace{m \vec{\omega} \times (\vec{\omega} \times \vec{r})}_{\text{Centrifugal force}}$$



$\vec{F}_{cor} \Rightarrow$ right deflection on northern hemisphere; left deflection on southern hemisphere

Affects wind direction:

